

# **Spinning Reserve from Pump Load: A Report to the California Department of Water Resources**

**April 2003**

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**SPINNING RESERVE FROM PUMP LOAD:  
A REPORT TO THE CALIFORNIA DEPARTMENT OF WATER RESOURCES**

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Transmission Reliability Program  
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## EXECUTIVE SUMMARY

The Oak Ridge National Laboratory, at the request of the California Energy Commission and the U.S. Department of Energy, is investigating opportunities for electrical load to provide the ancillary service of spinning reserve to the electric grid. The load would provide this service by stopping for a short time when there is a contingency on the grid such as a transmission line or generator outage. There is a possibility that a large part of the California Independent System Operator's (CAISO's) spinning reserve requirement could be supplied from the California Department of Water Resources (CDWR) pumping load.

Spinning reserve has never been supplied from load before, and rule changes would be needed to allow it. In this report, we are proposing that should the CDWR feel this concept has merit, we will pursue the needed rule changes with the North American Electric Reliability Council (NERC), the Federal Energy Regulatory Commission (FERC), the Western Electricity Coordinating Council (WECC), and the CAISO. This effort would enable a pilot project.

Presently, spinning reserve is provided by generation that is actually spinning but is operating at low power levels and can be ramped up quickly to provide reserve power. In a sense, this is an inefficient and environmentally unfriendly way of providing reserves because it requires the generator to operate at a low power level that may be inefficient and may discharge more pollutants per kW than operating at rated power. It would be better if this generation capacity were in a position to bid into the energy market. Providing an additional supply of spinning reserve would tend to reduce prices for both reserves and the regular electric energy market.

The CAISO is presently in the process of redesigning its market rules for ancillary services. The time is right to pursue this opportunity to supply spinning reserve from load. It is our hope that the CDWR will endorse this recommendation. We will then work with FERC, NERC, WECC, and the CAISO to obtain the needed rule changes. This project would provide the CDWR with another option in the complex process of obtaining its energy at the lowest possible cost, while at the same time providing more flexibility to the ISO and relief to the energy market. After this project is implemented in California, we hope that the practice spreads across the nation, allowing much more flexibility in energy markets and increasing the availability of reserve services.



## 1. CONCEPT OF SPINNING RESERVE FROM PUMPING LOAD

The concept of providing spinning reserve from the pump load is novel, but it builds on and complements the California Department of Water Resources's (CDWR's) existing energy management programs. CDWR's large megawatt size, coupled with its extensive knowledge of the California energy markets and its own loads, places it in an ideal position to evaluate the use of pumping load as spinning reserve and to design and implement a test project if the evaluation indicates that doing so is warranted.

Because of the high cost of electric power and the large amounts of power that CDWR both generates and consumes, CDWR is a sophisticated player in the California energy and ancillary service markets.

For CDWR, water delivery is the first priority, and any plans or modifications must consider this. The efficiency and reliability of water delivery cannot be compromised. However, CDWR's participation in the ancillary services market has provided an important revenue source in the past, and CDWR is always interested in exploring new ideas.

Spinning reserve has traditionally been supplied from generators. It can be thought of as providing insurance. The supplier is paid for having it available whether it is called for or not. It is only to be called in the event of a genuine system emergency, such as a lost transmission line or failed generator. It should only be called for infrequently, perhaps a few times per month. It should be restored to service rapidly (within 15 to 30 minutes) so that the power system is protected against the next contingency. Having the option to supply spinning reserve from load would provide flexibility in CDWR operations, provide another source of revenue, increase the reliability of California's electricity supply by increasing reserves, and decrease all customers' energy bills because reserve generation would be freed up to supply energy.

Spinning reserve could be supplied by load by simply turning off the load (e.g., a pump motor) when the reserve service is called for. North American Electric Reliability Council (NERC) rules have required that spinning reserve be supplied by generators in the past, but NERC recognizes that advances in communication and control technology now make it possible for load to supply spinning reserve. NERC has stated that it would be receptive to a waiver request. ORNL would work with the Federal Energy Regulatory Commission (FERC), NERC, Western Electricity Coordinating Council (WECC), and California Independent System Operator (CAISO) to work out the needed rule changes. FERC, NERC WECC, and CAISO rules are discussed in detail in Sect. 4.

ORNL has examined how CDWR pumping loads could be used to sell spinning reserve into the CAISO spinning reserve market. CDWR hourly power consumption information has been compared with CAISO hourly spinning reserve prices to determine how often CDWR could have sold spinning reserve, how much spinning reserve CDWR could have sold, and how much revenue this would have generated.

The results of the analysis are quite encouraging. Amazingly, it was found that the CDWR can supply more spin capacity than the CAISO needs for over 3000 hours per year. Based upon current market design, we expect that CDWR would be paid the market clearing price for spinning reserve whenever CDWR elected to stand ready to supply the reserves. There would be additional payments whenever the reserves were actually called upon to deploy. Total annual revenues of over \$11 million are possible. The results are discussed in detail in Sect. 2.



## 2. WATER PROJECT POWER CONSIDERATIONS

The Department of Water Resources (DWR) operates the State Water Project (SWP), which includes 18 pumping plants, 3 pumping-generating plants, and 5 hydroelectric power generating plants. The generation from the SWP's hydropower plants and from a coal-fired power plant in Nevada owned by DWR produces enough electricity in a normal year to supply about two-thirds of the power needed to serve the pumping load. In an average year, CDWR generates 5 billion kWh and uses 6 billion kWh of energy. CDWR generation does participate in the ancillary service markets (up and down regulation as well as contingency reserves) when the price makes it worthwhile. To the extent possible, CDWR generates on peak and pumps off peak. There is an exchange agreement with Southern California Edison (SCE) that recognizes the temporal variations in the value of electric power: CDWR receives more energy off peak than it exchanges with SCE during on-peak periods. Most of the required additional power comes from long-term contracts. The present power exchange contracts with SCE expire at the end of 2004. CDWR is planning now for new options.

There is a concern that the CAISO might not dispatch load-based contingency reserves (spinning and non-spinning) *only* to respond to contingencies (the sudden, unexpected loss of a generator or transmission line) or that it might not restore the reserves as quickly as NERC rules dictate (15 to 30 minutes). It will be important to develop contracts carefully so that spinning reserve is called for only in bona fide contingency situations and that it is restored to service quickly. Fortunately, those principles are in the best reliability interest of both the CAISO and CDWR. This issue is discussed further in Sect. 6.



### 3. CDWR PUMPING SYSTEM OPERATIONAL RESTRICTIONS AND SOFT START FOR LARGE MOTORS

#### 3.1 OPERATIONAL RESTRICTIONS

CDWR-owned generation facilities greatly reduce the cost of water pumping. They minimize the amount of power that must be purchased. Generation is scheduled to optimize its *value* in the energy markets rather than to directly supply the pumping loads. There are a number of significant environmental concerns, including water quality and wildlife habitat, for which regulatory constraints are imposed on operations for both hydropower generation and water pumping.

#### Pump Strings

CDWR’s pumping facilities are located along some 660 miles of aqueduct. The aqueduct is composed of river channels, reservoirs, canals, pipelines, and tunnels. There is little storage along much of the aqueduct, and in some locations, pumps operate as “strings” to keep the flow even. Turning one pump off at any plant to supply spinning reserve would cause a flow imbalance in the string, so pumps would have to be turned off and on at the same time at every plant. There may be sufficient storage, however, to accommodate the sale of spinning reserves (~30 minutes). Pumping is done primarily in off-peak hours, with as few strings on during on peak hours as possible.

Two pumping strings may present restrictions on the times that spinning reserve could be supplied. The first string is composed of the Buena Vista, Wheeler Ridge, Wind Gap, and Edmonston plants. Pumps may possibly be stopped individually on the string, but only for a maximum of 30 minutes. Dos Amigos, the water plant feeding into this string, and Pearblossom, one of the water plants on the output of the string, may be capable of independent interruption for 2 hours before water storage limits are reached. The second pumping string is Las Perillas and Badger Hill. It is possible that each of these pumps could be stopped individually for a period of only 30 minutes.

When a pumping string is called upon to supply spinning reserve, it is reasonable to assume that only the largest pump in each plant of the string will be stopped. The pump motor ratings for each of the pumping string plants are as follows:

#### First String

Buena Vista	Pumps 1–3:	8,500 hp	Pumps 4–10:	17,000 hp
Wheeler Ridge (Teerink)	Pumps 1–3:	10,000 hp	Pumps 4–9:	20,000
Wind Gap (Chrisman)	Pumps 1–3:	22,000 hp	Pumps 4–9:	
Edmonston	Pumps 1–14:	80,000 hp	(These pumps provide a large lift.)	

#### Second String

Las Perillas	Pumps 1–3:	350 hp	Pumps 4–6:	1000 hp
Badger Hill	Pumps 1–3:	1000 hp	Pump 4:	750 hp
			Pumps 5–6:	3000 hp

The pump motors, in general, are designed for multiple starts per day. A rule of thumb has been two starts with a 30-minute cooldown period between them, then a 1-hour cooldown. The large Edmonston pumps, 80,000 hp, use motor generator sets to assist in starting; these motors are not started across the line at rated voltage and frequency. The motor generator sets provide a form of soft start, where the motor is started at a reduced frequency. Soft starting is discussed further in Sect. 3.4.

### **3.2 RESTRICTIONS DUE TO SOUTH BAY AND PIPED SYSTEMS**

The South Bay aqueduct is operating at near rated capacity to satisfy demand in the South Bay area of San Francisco. This aqueduct was one of the first constructed, built in the early 1960s. It includes the South Bay and Del Valle pumping plants. These plants are sometimes operated at near full pumping capacity to satisfy demand, and spin would probably not be available during some months of the year.

In addition, some pumping plants are connected only by pipe, not by canal. An example is the Coastal Branch where the Badger Hill, Devil's Den, Bluestone, and Polonio Pass plants combine to pump water over an elevation of 2500 ft. Interrupting pumps may present hydraulic concerns during some loading conditions.

### **3.3 PUMP-BACK RESTRICTIONS**

In some cases, CDWR will pump into reservoirs either to fill the reservoir for water supply during off-peak hours or simply to provide energy storage so that the pumps can be operated as generators during on-peak hours. These decisions are made on a daily basis using an avoided-cost analysis. Spinning reserve could be factored into the analysis. Typically, spinning reserves prices fluctuate with energy costs, but there have been times when spin prices have been high in the middle of the night in the California market. In these cases, there would be a significant opportunity for revenue, as well as an opportunity to reduce the high price for spinning reserve by providing it from other sources.

### **3.4 SOFT STARTING FOR LARGE MOTORS**

Presently, the Teerink and Chrisman pump motors are started "across the line" but unloaded (pumps running in air instead of water). The motor and pump accelerate to synchronous speed in about 2 seconds. Considering that the rotational inertia of the pump and motor is about one million foot pounds, and that this inertia is accelerated to synchronous speed in 2 seconds, offers a sense of the forces involved with an across-the-line start.

A soft start is a reduced-voltage, reduced-frequency start. It starts the motor more slowly with reduced stress. A form of soft start is provided for the large Edmonston pump motors using the motor-generator set. This soft start is not used on the other pump motors at the other pumping plants. The motors at Teerink and Chrisman are rated at 10,000, 20,000, 22,000, and 44,000 hp. Although smaller than the motors at Edmonston, these are not small motors by any means, and they are subjected to large stresses when starting.

Large synchronous motors are typically equipped with damper (or amortisseur) windings used for starting. The damper winding performs the same function as the squirrel cage winding in the rotor of an induction motor. It is used to create torque when the rotor is slipping (running behind synchronous speed) during starting. A synchronous motor started across the line is started as an induction motor using the damper winding, and the field is switched on only when it is running near synchronous speed. Across-the-line starting results in high inrush current and stress on the circuit breaker and windings. A soft starter for a synchronous machine usually operates the machine as a synchronous machine at variable frequency. This means that the field is excited from zero speed, but the starting frequency is quite low and is raised gradually.

Although these motors have been designed to start at rated voltage and frequency, a tremendous amount of force is placed on the amortisseur winding when the motor is started. CDWR has had to rebuild and reblock amortisseur windings in Teerink and Chrisman pump motors in the past. The exact cost of motor degradation has been the subject of analysis and discussion, but this may be a location where we would want to consider a soft start.



The soft-start method is summarized as follows.

Typically, a soft starter, or converter, is set up to start a number of motors at a plant. The soft starter is a variable-frequency drive that converts both frequency and voltage. Each motor has two circuit breakers feeding it, one on the soft starter output bus and one on the main power supply bus or line. To start a motor, it is connected to the soft starter, accelerated up to speed, synchronized to the line, and then switched over to the line. Reducing voltage means less torque is applied to the motor shaft; reducing frequency means that the motor accelerates more slowly. Once the motor is running and synchronized, the soft starter is available to start the next motor.

There are two basic synchronizing methods. In the first method, the motor is accelerated slowly with reduced magnetic flux (using reduced input voltage) to a speed a few percentage points above synchronous speed. The converter is then disconnected from the motor. As the motor coasts back down to synchronous speed, it is fully excited, and it is connected to the line supply at the instant the motor voltage and phase coincide with those of the line supply. This transition is monitored and controlled by a synchronizing device. In the second method, the frequency is raised slowly until the speed reaches 95% of the synchronous speed. The synchronizing device controls the speed setpoint until the synchronizing point is precisely reached. The converter is then disconnected, and the motor circuit breaker is closed. The amortisseur winding will not provide enough torque itself to accelerate both the motor and pump impeller, and the motor's field winding will also need to be controlled during starting.

Because the soft starter operates for only two or three minutes, it does not have to have the same power rating as the motor. About 10 to 20% of rated motor horsepower is probably a good estimate of the rating needed for a starter for a large synchronous motor driving a centrifugal pump. As an example, Siemens manufactures load-commutated inverters in sizes up to 100,000 hp. For a 44,000-hp motor, the largest motor at Chrisman, a starter rated at 9 MW should be adequate. This is one of the standard sizes that Siemens manufactures.

Siemens has provided a budgetary estimate for a 9-MW starting frequency converter, which is attached as Appendix A. The estimate for a 9-MW load-commutated current source inverter includes the input circuit breaker and transformer, the starting frequency inverter, control units for the existing field excitation controller, the synchronizing unit, the output transformer, and 11 output circuit breakers that would be used to connect to each pump motor. The cost for the entire system would be around \$1.5 million for one pumping plant. The estimate was done for the Chrisman plant, and the same system could be used for the smaller motors at the Teerink plant. It may be advantageous to use identical equipment for both sites for spare parts and economy in design and manufacture. The total installed cost would probably be around \$2.25 million per plant.



## **4. RESERVE REQUIREMENTS**

The electric power system is unique in that aggregate production and consumption must be matched instantaneously and continuously. Several types of controllable reserves are maintained to help the system operator achieve this required generation/load balance. Regulating reserves compensate for the continuous random minute-to-minute fluctuations in load and uncontrolled generation. Frequency-responsive reserves compensate for the frequency deviations. The daily cycling of load is compensated through load following and generator dispatch. Finally, sudden failures of generation and transmission are addressed with three additional reserve products: spinning reserve, non-spinning reserve, and supplemental or replacement reserve (collectively referred to as “contingency reserves”).

Conceptually the generation/load balance can be maintained by controlling generation, load, or both. Historically, system operators have tended to control generation almost exclusively. Generators are typically in the business of providing their services to the power system, so their business models (whether they are owned by an integrated utility or are independent) accommodate following system operator directives. Communication and control technology also has made it easier to monitor and control a few large resources than numerous smaller resources. Consequently, the rules governing how the power system is operated were developed at a time when large generators were essentially the only resources available to support system reliability. Rules were prescriptive as to the actions to be taken and the technologies to be used, rather than being results oriented (i.e., performance based).

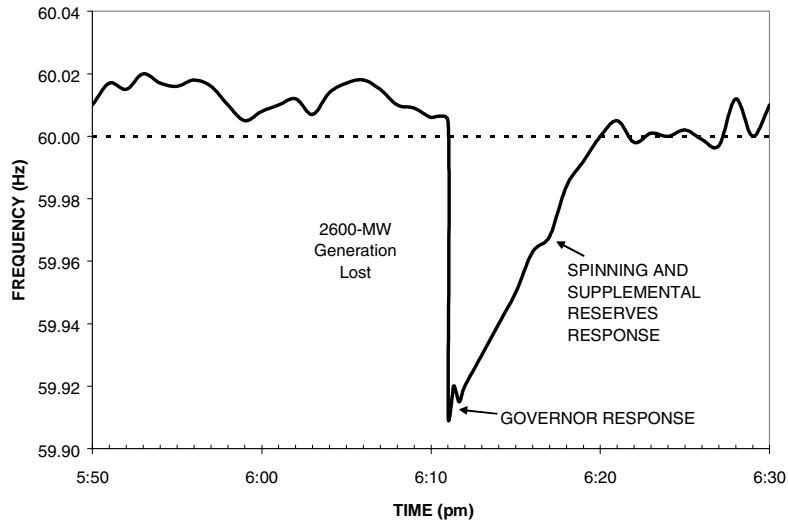
Restructuring has changed the business relationships between generators and the system operator. Technology has advanced to allow loads to be responsive. Energy costs have risen and have become more volatile from hour to hour, providing incentives for loads to respond. Rules established by regulators and technical organizations are being changed to accommodate this new set of circumstances.

### **4.1 TECHNICAL REQUIREMENTS**

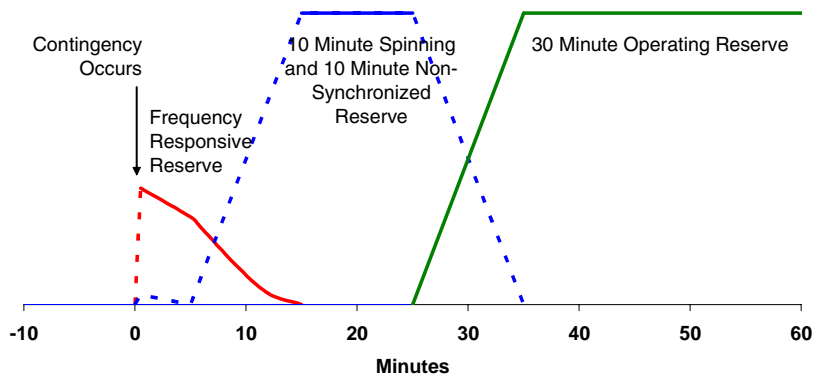
While responsive load theoretically can provide almost any service the power system requires (black start may be the only exception), most loads are best suited to provide contingency reserves. Contingency reserves restore the generation/load balance after the sudden unexpected loss of a major generator or transmission line. Power system frequency drops suddenly when generation trips, as shown in Fig. 4.1. In these instances, there is no time for markets to react. In the case shown in Fig. 4.1, frequency-sensitive generator governors responded immediately to stop the frequency drop. Spinning and supplemental reserves successfully returned frequency to 60 Hz within 10 minutes. Power systems typically keep enough contingency reserves available to compensate for the worst credible event (contingency). This is typically the loss of the largest generator or the largest importing transmission facility. In Texas, the simultaneous loss of two nuclear plants is credible (as shown by the event recorded in Fig. 4.1), so the Electric Reliability Council of Texas requires over 2600 MW of contingency reserves. Frequency-responsive, spinning, supplemental, and replacement reserves operate in a coordinated fashion, as shown in Fig. 4.2.

### **4.2 REGULATIONS AND POLICIES**

Although the general concepts of system operations and reliability are well established, implementation details continue to evolve as the industry is restructured. FERC, NERC, WECC, and the CAISO all have rules and procedures that govern contingency reserve requirements.



**Fig. 4.1. Governor response and contingency reserves successfully restored the generation/load balance after the loss of 2600 MW of generation.**



**Fig. 4.2. Contingency reserves provide a coordinated response to a sudden loss of supply.**

These rules, and even the specific service names, are not yet consistent among organizations; but the trend toward open, technology-neutral market-based solutions is clear.

#### 4.2.1 Federal Energy Regulatory Commission

FERC, in its notice on Standard Market Design (SMD) (FERC 2002a), shows a clear preference for market-based solutions for energy supply and reliability. It also encourages demand participation on an equal footing with generation. The proposed SMD specifies day-ahead markets for spinning and supplemental reserves but not for the 30-minute replacement reserve. These markets are to be integrated with the energy market. FERC also proposes operation of real-time markets for ancillary services.

#### 4.2.2 North American Electricity Reliability Council

In its most recent operating manual (NERC 2002), NERC has continued its move away from prescriptive requirements for operational practices to relying more on performance standards. Policy 1, *Generation Control and Performance*, specifies two standards that control areas must meet to maintain reliability in real time.<sup>1</sup> The Control Performance Standard (CPS) covers normal operation, and the Disturbance Control Standard (DCS) deals with recovery from major generator or transmission outages.

Policy 1 still discusses the resources that control areas will need to meet the performance standards. Each control area is required to have sufficient operating reserves to “account for frequency support, errors in load forecasting, generation loss, transmission unavailability, and regulating requirements.” It defines “sufficient operating reserves” as “the capacity required to meet the Control Performance Standard (Section A), Disturbance Control Standard (Section B), and Frequency Response Standard (Section C) of this Policy.”<sup>2</sup>

NERC’s DCS is a performance measure; it specifies that the control area must recover the generation/load balance within 15 minutes of the start of a contingency. To provide resources to meet the DCS, Policy 1 defines contingency reserves as a subset of operating reserves:

Each CONTROL AREA shall have access to and/or operate CONTINGENCY RESERVES to respond to DISTURBANCES. This CONTINGENCY RESERVE is that part of the OPERATING RESERVES that is available, following loss of resources by the CONTROL AREA, to meet the Disturbance Control Standard (DCS). CONTINGENCY RESERVE may be supplied from generation, controllable load resources, or coordinated adjustments to INTERCHANGE SCHEDULES.<sup>3</sup>

Policy 1 goes on to state that each regional reliability council will establish contingency reserve policies covering the minimum reserve requirements, the mix of spinning and supplemental reserves, and “the limitations, *if any*, upon the amount of interruptible load that may be included” (emphasis added). There is a further requirement that each control area or reserve sharing group carry at least enough contingency reserves to cover the most severe single contingency. NERC requires that reserves be restored within 90 minutes of deployment.

There are two important points here. First, the composition of the reserves is not specified. NERC no longer requires spinning reserves to come from generation (although regional councils are not prohibited from setting that requirement).<sup>4</sup> Second, contingency reserves are to be used to meet the DCS standard. That is, they are to respond to contingencies. If they are used to respond to forecast errors, generation or transmission maintenance, or other such problems, they are not available to respond to contingencies. This latter distinction is important to responsive loads because it has a large impact on the response duration. Oddly, as we will discuss in greater detail, responsive loads, unlike most generators, care about what the response is to be used for.

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<sup>1</sup>Policy 1 contains five additional standards: *Frequency Response and Bias*, *Time Control*, *Automatic Generation Control*, *Inadvertent Interchange*, and *Surveys*.

<sup>2</sup>The frequency response standard will likely evolve into a performance standard similar to CPS and DCS, but it is currently still only a specification of how to set the frequency bias.

<sup>3</sup>NERC capitalizes terms in its policies that have NERC-defined meanings.

<sup>4</sup>The “Terms and Definitions” in the NERC Operating Manual have not yet been updated, and spinning reserve is still defined as “unloaded generation that is synchronized and ready to serve additional demand.”

### 4.2.3 Western Electricity Coordinating Council

WECC specifies the minimum amounts of contingency reserve each control area in the West must carry (2002).

WECC sets the minimum contingency reserve requirement as the greater of (1) the largest contingency or (2) 5% of the load served by hydroelectric resources, plus 7% of the load served by all other resources, with additions related to nonfirm energy imports and firm exports of reserves. WECC requires that at least 50% of contingency reserves be spinning, primarily to respond to frequency deviations.

These reserves are required to meet the DCS. WECC (2002) describes the DCS as follows: “Each control area or reserve sharing group shall include events that cause its Area Control Error (ACE) to change by at least 35% of the maximum loss of generation that would result from a single contingency.” The recovery from DCS events must meet the following criterion: “Following the start of a disturbance, the ACE must return either to zero or to its pre-disturbance level within the time specified in the Disturbance Control Standard currently in effect in NERC Policy 1 [15 minutes].”

After responding to a contingency, the reserves must be restored in order to be prepared for the next contingency. WECC requires that reserves be restored within one hour: “After the occurrence of any event necessitating the use of operating reserve, that reserve shall be restored as promptly as practicable. The time taken to restore reserves shall not exceed 60 minutes” (WECC 2002).

WECC does not allow responsive load to provide spinning reserve; spinning reserve must come from generation. “Spinning Reserve—Unloaded generation which is synchronized and ready to serve additional demand. It consists of Regulating Reserve and Contingency Reserve” (WECC 2002). Responsive load, which can be interrupted within 10 minutes, is allowed to provide non-spinning reserve.

### 4.2.4 California Independent System Operator

The CAISO further refines the NERC and WSCC reserve requirements and operates day-ahead and hour-ahead markets to obtain these reserves hourly. The CAISO specifies three contingency reserves:

**Spinning Reserve:** Reserve capability available within 10 minutes from on-line generating capacity.

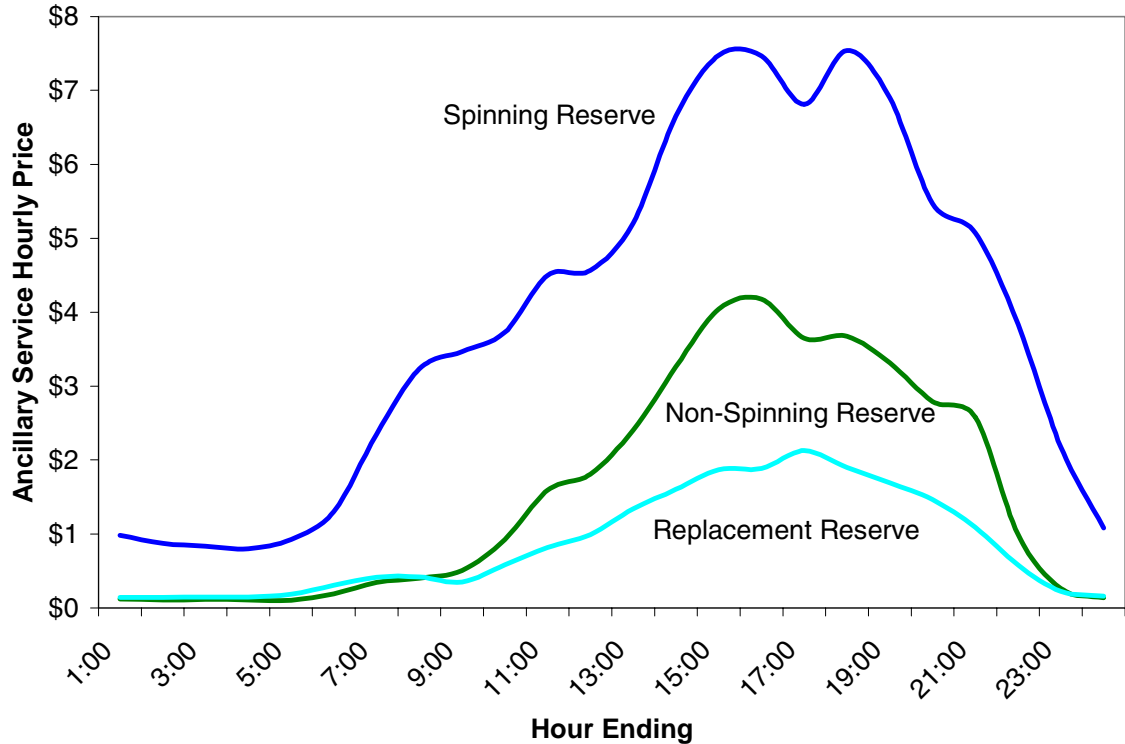
**Non-Spinning Reserve:** Reserve capability available within 10 minutes from

- Off-line generation capacity
- Interruptible load and/or exports
- On-demand imports
- Excess spinning reserve

**Replacement Reserve:** Reserve capability available within 60 minutes from on-line or off-line generating capacity.

The CAISO echoes the WECC requirements for the amount of reserves and the percentage that must be spinning. Replacement reserves are procured to meet the difference between the scheduling coordinator’s scheduled load and the ISO-forecast load.

The CAISO required 865 MW of spinning and non-spinning reserves in 2002, on average. The hourly peak requirement was 1376 MW for each service, and the hourly minimum requirement was 585 MW. Markets are run for spinning reserve, non-spinning reserve, and replacement reserve.<sup>5</sup> The CAISO ancillary service markets are locational, and prices diverge when there is transmission congestion. Annual average prices for the three contingency reserves are shown in Fig. 4.3. These prices show the expected daily pattern where prices are low at night and high in the afternoon. Also, spinning reserve, the highest-quality service, is 2.5 times as expensive, on average, as non-spinning reserve. Figure 4.4 shows the same pattern for July, when prices were considerably higher.

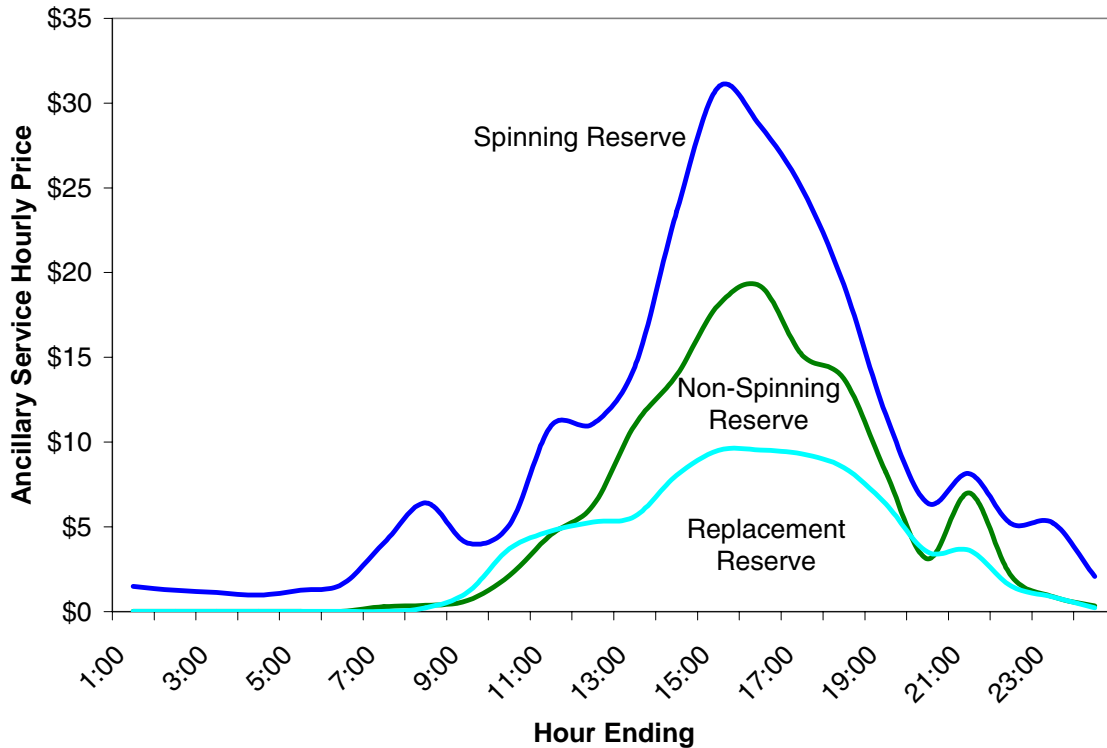


**Fig. 4.3. Average hourly CAISO contingency reserve prices follow an expected daily pattern with spinning reserve, the fastest service, having the greatest value: 11/2001–10/2002.**

### Spinning Reserve Capacity and Energy Bid Components

Bids to supply spinning and non-spinning reserves to the CAISO have two parts: capacity and energy. Only the capacity bids are shown in Figs. 4.3 and 4.4. Bids are submitted for each hour that the supplier wishes to sell reserves to the system. The market clears based upon the capacity bid prices. All successful suppliers are paid the hourly capacity price for standing ready to supply reserves if they are needed. The energy bids are used only if reserves are actually deployed. In that case, reserves are selected for actual deployment based upon their energy bids, with the cheapest reserves being deployed more frequently. Each supplier is paid its energy bid price when it is utilized. Capacity and energy bids should be based upon their respective expected costs (CAISO 2003c).

<sup>5</sup>The CAISO runs separate markets for generation and load for non-spinning reserve and replacement reserve, although the prices are the same. The CAISO also runs markets for regulation up and regulation down.



**Fig. 4.4. The daily pattern of hourly CAISO contingency reserve prices for July of 2002 showed the same expected pattern, but those prices were considerably higher than the annual average hourly prices shown in Fig. 4.3**

### Grid Management Charge

The CAISO obtains the funds required for its operation from the grid management charge (GMC). There are three parts to this charge: one for recovering the ISO cost of providing control area services, a second for providing congestion management and transmission access services, and the third for recovering the cost of providing a market for the real-time energy and ancillary service transactions. This third GMC “market participation” charge applies to every purchase or sale of real-time balancing energy or ancillary service through the CAISO market. Both suppliers and loads pay this GMC charge on each megawatt-hour of ancillary service reserve that clears through the CAISO ancillary service market (CAISO 2000, CAISO 2003b, and Hoffman 2003).

This portion of the GMC charge was \$0.975/MWh in 2002 (and is \$1.30/MWh in 2003). Since both buyers and sellers are charged, this represented a \$1.95/MWh surcharge on spinning and non-spinning reserves for 2002. The price of spinning reserve averaged \$3.89/MWh and the price for non-spinning reserve averaged \$1.57/MWh in 2002. Hence the GMC charge is a dominant consideration. The market clearing price for spinning reserve was *below* the GMC (\$0.975/MWh) for 4037 hours in 2002. The market clearing price for non-spinning reserve was *below* the GMC for 6166 hours in 2002. It is not clear why generators were willing to sell reserves during these hours, since they were losing money. The GMC does *not* apply to self-provision of ancillary services. Consequently, self-provision of reserves has increased in importance. About half of the reserves are self-provided. The CAISO is working on market redesign for 2004. It is hoped that the GMC for ancillary services will be addressed at that time.

There are two significant GMC consequences for CDWR provision of spinning reserve from its load. First, use of CDWR responsive load may be an attractive way for CDWR to meet its own spinning reserve obligation. The reserve value would then be the sum of the GMC and the market



clearing price. Second, CDWR might wish to enter into arrangements with other load-serving entities to provide their spinning reserve requirements, thus allowing them to avoid the GMC. We did not analyze these opportunities further. We hope the GMC will be redesigned so that it does not influence the reserve markets, as is the CAISO's stated intent.

### **CAISO Market Redesign**

The CAISO is actively redesigning the ancillary service markets. Some redesign will be implemented in the fall of 2003; more extensive redesign is expected in 2004. Redesign details are not yet available, and an analysis of proposed changes is beyond the scope of this report. The important point is that new CAISO market rules need to be evaluated as they are implemented to determine their impact on CDWR. Also, CDWR should actively participate in CAISO market redesign to ensure that the new market rules accommodate CDWR needs and capabilities.



## 5. SUPPLYING SPINNING RESERVE FROM CDWR PUMPS

We modeled interactions between the CAISO spinning and non-spinning reserve markets and the CDWR pumping loads to determine how much reserve capacity could be supplied by CDWR pumps and what the value would be. This preliminary modeling may not have captured all of the limitations associated with each pumping station. The use of time-domain modeling ensures that these limitations can be easily identified and included in subsequent analyses.

### 5.1 MODELING CONTINGENCY RESERVE SUPPLIED BY CDWR PUMPS

We developed a Fortran-based, time series computer model to help evaluate the viability of using CDWR large pumps to supply contingency reserves to the California ISO power system. It utilizes hourly pumping loads at each pumping station. It combines these with hourly spinning and non-spinning reserve requirements and prices to determine the hourly revenue for each pumping station. The model is built to use locational reserve prices specific to each pumping station location. Limited resources prevented obtaining locational prices for this preliminary study. NP15 prices were used for all locations.

A minimum acceptable price can be specified for each pumping station. Reserves are not sold, and the pumping station does not incur the risk of having to curtail operation, unless the hourly reserve price exceeds this established minimum.

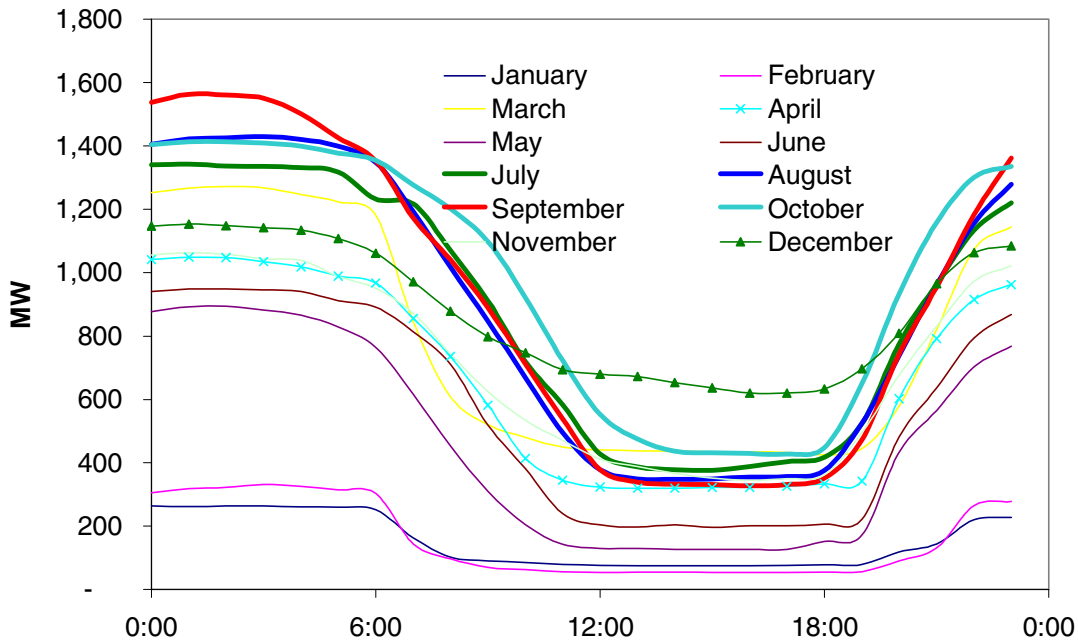
The model determines, for each hour and each pumping station, how much spinning and non-spinning reserve is available, how much reserve is sold, and how much revenue is generated. Results are summarized, providing total revenue per pumping station. Detailed information is also available concerning exactly when, and under what conditions, supplying reserves is most attractive.

The model can be run for any length of time. For this study, a full year was modeled. Hourly CDWR load data were obtained for each pumping station for 1999 from CDWR. Ancillary service price data were obtained for 2002 from the CAISO OASIS web site (CAISO 2003a). Disparate years were used because it was felt that 1999 was a more typical water year, while 2002 provided more ancillary services prices that were not distorted by dysfunctional markets. Unfortunately, the California power markets were not well-behaved until various market reforms were introduced in 2000 and 2001. The power markets settled down in the late summer of 2001 and appear to have been performing well since.

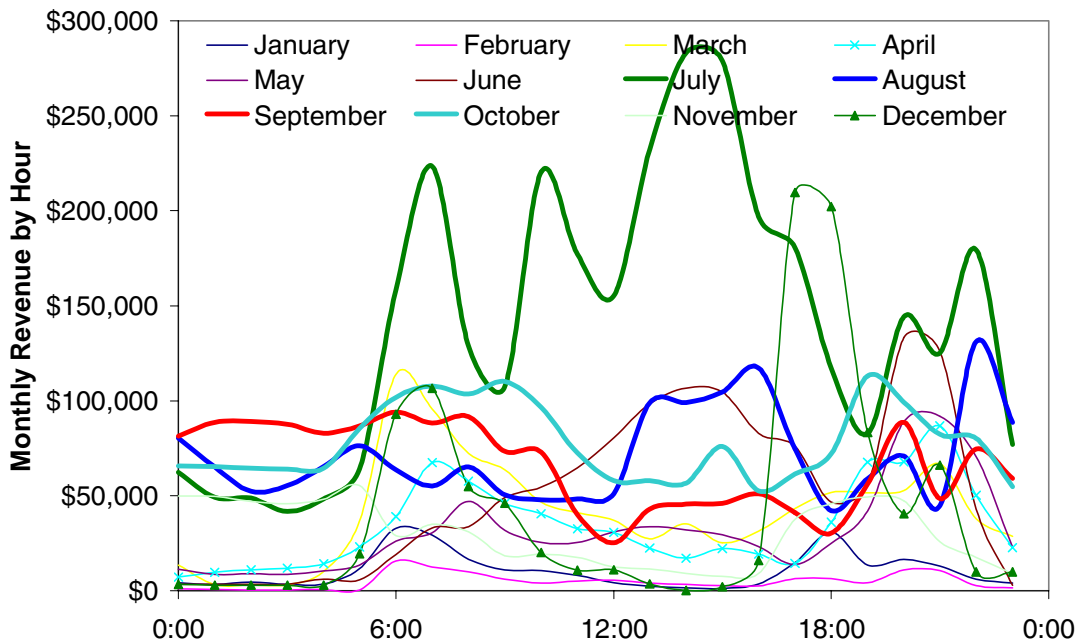
### 5.2 RESULTS

For the CDWR, water delivery is its first priority, and any plans or modifications must carefully consider this priority. The efficiency and reliability of the water delivery cannot be compromised. However, to the extent possible, CDWR pumps during off-peak hours to reduce pumping costs, as shown in Fig. 5.1.

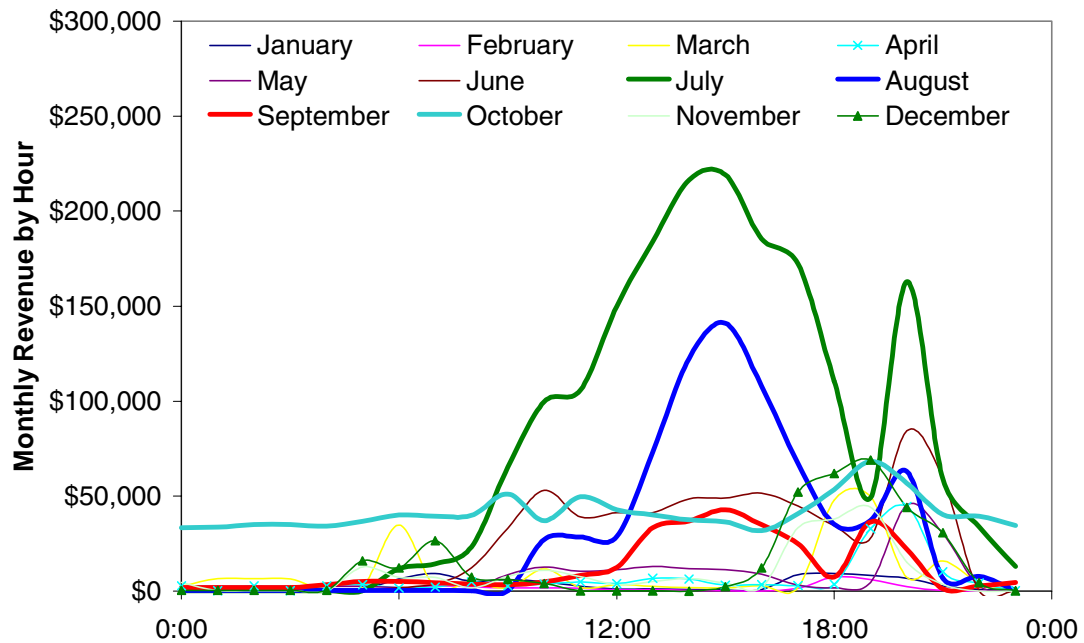
Optimizing power purchases to minimize energy costs would appear to limit opportunities for selling contingency reserves. Contingency reserve prices tend to track energy prices and are highest in the middle of the day, as was shown in Figs. 4.3 and 4.4. Still, modeling the hourly CDWR load and CAISO ancillary service prices shows that there are significant opportunities. The modeling reveals that CDWR could have made \$12.9 million selling spinning reserve in 2002 (with 1999 water conditions). (This calculation was made using the actual price for spinning reserve and the number of megawatts the CDWR was using for pumping by the hour.) Non-spinning reserve would have yielded only \$5.6 million. Figure 5.2 shows the hourly revenue by month for spinning reserve; Fig. 5.3 shows the reduced revenue available from non-spinning reserve.



**Fig. 5.1. CDWR is a sophisticated power purchaser, minimizing costs by pumping during off-peak times whenever possible.**



**Fig. 5.2. Total annual revenue from selling spinning reserve could have been \$12.9 million in 2002 with 1999 water conditions.**

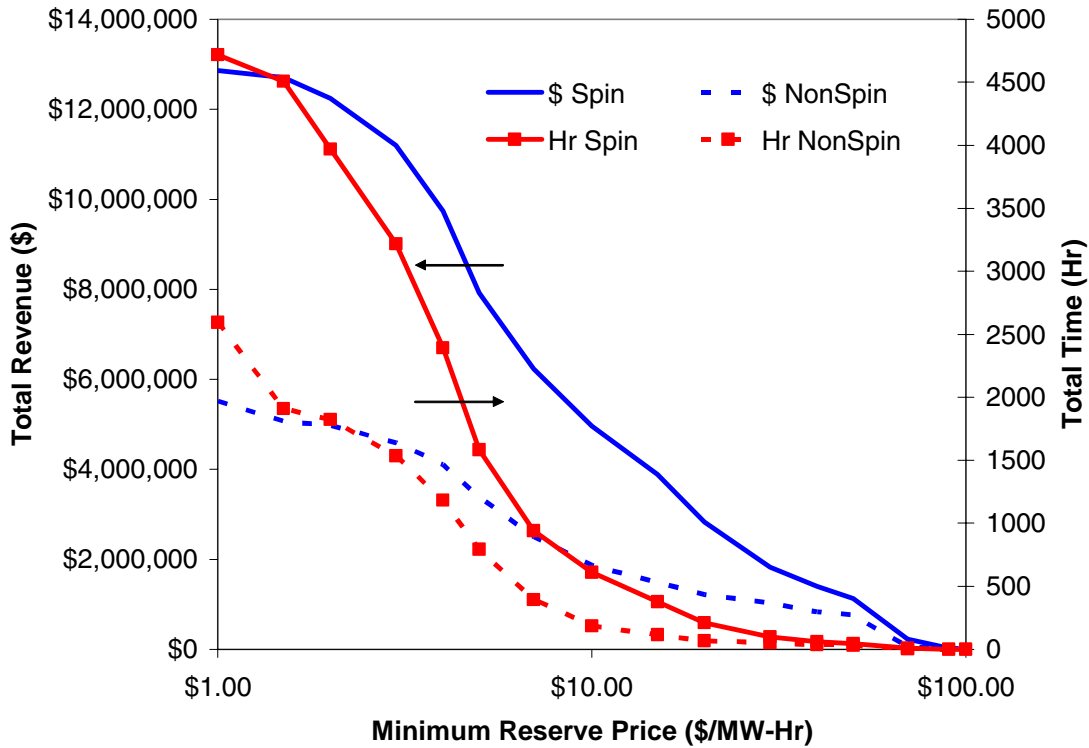


**Fig. 5.3. Non-spinning reserve revenue would have been only \$5.6 million for the same 2002 ancillary service prices and 1999 water conditions.**

Spinning reserve that could be supplied from CDWR pumps represents not only significant potential revenue but also a significant amount of the total California spinning reserve requirement. In fact, CDWR has sufficient potentially responsive load to supply 62% of the CAISO spinning reserve requirements under the conditions modeled. CDWR pumps had sufficient hourly capacity in operation to supply 100% of the spinning reserve requirements for 3292 hours in 2002.

### Minimum Price

At times, the contingency reserve prices are quite low. CDWR might not want to expose its pumps to the risk of being curtailed unless it were receiving enough compensation to justify the risk. Determining what minimum price is acceptable requires assessing the probability of actually being called on to respond and the costs CDWR will incur to respond. That analysis is beyond the scope of this study. We did, however, calculate both the revenue reduction and the reduction in the number of hours for which CDWR would be exposed to curtailment risk as it raised the minimum acceptable price for both spinning and non-spinning reserves. Figure 5.4 shows that both the revenue and exposure hours drop as the minimum price rises, but that the exposure hours drop faster than revenue. Raising the minimum acceptable spinning reserve price from \$1/MWh to \$3/MWh, for example, drops revenue by 13% (from \$12.8 million to \$11.2 million), but it drops the curtailment exposure by 32% (from 4718 hours to 3218 hours). It is likely that optimized minimum acceptable reserve prices will vary from plant to plant, from pump to pump, and from time to time, depending on the varying operating conditions.



**Fig. 5.4. Setting a minimum acceptable price for selling spinning or non-spinning reserve reduces revenue, but it also reduces the exposure to curtailment.**

### Revenue from Individual Pumps

The results presented so far are for the aggregated CDWR pumping load. That aggregated load is, of course, composed of individual pumping stations and individual pumps. CDWR supplied hourly loads for each pumping station, making it possible to evaluate individual stations and determine which ones offer the greatest potential benefit. CDWR did not supply hourly loads on each pump, but we synthesized individual pump loads by assuming a loading order for the pumps within each pumping station. This analysis was designed to determine how much revenue each individual pumping station and each individual pump could generate if that station and pump had response capability. This helps identify which pumps are potentially the best candidates for initial testing.

We modeled provision of both spinning and non-spinning reserve. We then sorted the individual pump revenues by total revenue for the year and by revenue per megawatt of pump size. This identified both the pumps that can generate the greatest revenue and pumps that can generate the greatest revenue normalized for pump size. These results are tabulated and presented in Appendix B.

Tables B.1 and B.2 (Appendix B) show the greatest revenue is available (for the conditions modeled) from the large Edmonston pumps (80,000 hp); Edmonston has four of the five pumps with the largest revenue potential for both spinning reserve and non-spinning reserve. When the evaluation is performed based upon revenue per megawatt of pump size, the smaller South Bay pumps (1300–2500 hp) are three of the five highest revenue producers. The Edmonston pumps are 26th and 33rd in the spinning and non-spinning reserve stacks on the basis of pump capacity in megawatts.

### **Spinning Reserve Capacity and Energy Bid Components**

Bids to supply spinning and non-spinning reserves to the CAISO have two parts: capacity and energy. Bids are submitted for each hour that the supplier wishes to sell reserves to the system. The market clears based upon the capacity bid prices. All successful suppliers are paid the hourly capacity price for standing ready to supply reserves if they are needed. The energy bids are only used if reserves are actually deployed. In that case, reserves are selected for actual deployment based upon their energy bids, with the cheapest reserves being deployed more frequently. Capacity and energy bids should be based upon their respective expected cost.

The capacity bid should be based upon the expected incremental cost to supply spinning reserve each hour from each pumping facility. These costs will include the cost of any change in operations that is necessary to be ready to respond—for example, operating with a more flexible, faster-responding, but less efficient pumping configuration. Bids are likely to vary from location to location and from hour to hour as operating conditions vary. Capacity bid costs are likely to be fairly low.

Revenue from selling contingency reserves needs to be high enough to cover any capital costs incurred in order to develop the capacity to supply the contingency reserves. The hourly capacity bids should not, however, include these costs since they are sunk costs. It is to be hoped that the market clearing prices (the actual prices received) for the contingency reserves will be high enough to recover the capital costs and turn a profit.

The energy bid should be based upon at least three factors: the cost of energy required to replace the energy being supplied in the reserve deployment, costs associated with disrupted operations, and the CAISO's GMC. The first and third are relatively easy to estimate. The second is more difficult.

First, when the load curtails operation in response to a contingency reserve deployment command from the system operator, the generator that had been supplying the load continues to operate. The load pays for the energy that it did not receive and that went to the system. The energy bid needs to recover the cost of this energy. But recovering the cost of the energy that the load did not consume is not enough. The load still has to accomplish the work (pump the water) that it had intended to accomplish with the energy it just gave to the system. Since energy operations were already optimized to minimize costs, it is likely that the replacement energy will be more expensive, perhaps requiring more on-peak purchases.

Second, there may be some additional costs associated with responding to the reserve deployment. Any operational cost could be minimized by making the response part of the standard set of services that the CDWR provides to the ISO. There will naturally be costs involved in any programming changes that are needed for the pump supervisory control and data acquisition (SCADA) system, and perhaps for certifying the pumps as official spinning reserve providers; but these should be one-time costs and should not be significant. Because the pumps should be called upon only two or three times per month, motor degradation from more frequent starts should be minimal. Larger motors could be supplied with soft starters, as described in Sect. 3.4.

Finally, the CAISO finances its operations through the GMC. A portion of the GMC is assessed on each megawatt hour of energy. In 2003, this charge is \$1.30/MWh. It needs to be added to the energy portion of the contingency reserve bid.





## **6. RECOMMENDATIONS**

### **6.1 PUMP SELECTION**

Table B.1 (Appendix B) indicates that significant revenue is available from the string of Buena Vista, Wheeler Ridge (Teerink), Wind Gap (Chrisman), and Edmonston. However, these pumps probably could not be stopped individually for 2 hours because there is not enough water storage in the string. If the CAISO agrees to a 30-minute interruption for spinning reserve, then the pumps could supply it individually, because they could be stopped individually for 30 minutes. If the CAISO requires spinning reserve to be supplied for 2 hours, then one pump in each plant in the entire string would be stopped to supply the service. The CDWR would make the decision as to whether the 2-hour interruption was possible.

As a second option, spin could be supplied from Las Perillas and Badger Hill string. Also, the revenue available per megawatt is quite attractive for the pumps at South Bay, Polonia Pass, Devil's Den, Bluestone, Barker Slough, Badger Hill, and many others. These may be attractive for a pilot program. As mentioned earlier, the South Bay aqueduct is operating at near rated capacity, and spin probably would not be available during some months of the year. In addition, the Badger Hill, Devil's Den, Bluestone, and Polonia Pass plants combine to pump water over a substantial elevation, so interrupting pumps might present hydraulic concerns. Again, it may be possible to stop one pump in each plant in the string. This decision would be made by the CDWR after analysis. This decision will be a factor of whether the duration of the pump outage is 30 minutes or 2 hours. The duration will be decided in the upcoming CAISO ancillary services market redesign.

### **6.2 NEEDED RULE CHANGES**

At the present time, NERC has indicated that it would be responsive to a waiver request to supply spinning reserve from load, and FERC has changed its definition of spinning reserve to allow it to be supplied from load. Now that the CAISO is actively redesigning the ancillary service markets, it is appropriate to approach WECC and request a waiver to supply spinning reserve from load and to allow it to be supplied for a period of 30 minutes. We anticipate that WECC would be responsive to this request. We believe that NERC would support it. After we have obtained WECC approval, the request could be made to the CAISO to include this change in the redesign. Even if the CAISO is not able to make the change from 2 hours to 30 minutes, we believe that it would be amenable to allowing spinning reserve to be supplied by load.

If we obtain a rule change or waiver from NERC and WECC that permits spinning reserve to be supplied from load for a period of 30 minutes, it would provide a strong motivation to the CAISO to allow the change.

The 2-hour sustained off-time requirement may be difficult to meet. It will limit the locations at which and times during which the CDWR is able to respond. It may be in the CAISO's interest to reduce the 2-hour requirement to make spinning reserve much easier to supply from load.

As discussed in Sect. 4, NERC and FERC are now essentially in support of the concept of supplying spinning reserve from load. If CDWR concurs that this proposal to supply spinning reserve from load has merit and should be pursued, we will document the NERC and FERC positions and prepare a formal request to the CAISO and WECC for the capability to supply spinning reserve from load, and for this service to be supplied for a time frame of 30 minutes. This request could be considered during the redesign of the ancillary services market.

One argument for a shorter deployment time is that replacement reserves are required to be on within 1 hour, so they should replace the spinning and non-spinning reserves. Another possibility is that CDWR might offer to be able to redeploy in the unlikely event that another contingency occurs within the 2 hours. It might be possible to shut down the high-value-per-megawatt pumps that are not located in the strings for 2 hours.

## 7. PROPOSED STEPS

If CDWR agrees that the proposed rule revision will add a useful level of flexibility to its operations and will provide a significant new revenue source, ORNL will proceed with the following steps to initiate a rule change.

- ORNL will confirm with FERC that the existing rule for spinning reserve allows it to be provided by shedding load, or that a rule change could be obtained through a waiver. The waiver would need to be initiated through WECC. Confirm also that the existing rule allows a duration of only 30 minutes.
- We will confirm with NERC that the existing rule for spinning reserve allows it to be provided by shedding load, or that a rule change could be obtained.
- WECC requires that the reserves be restored in 1 hour and that spinning reserve must be supplied by generation. We will make a presentation to WECC on the concept, and we will request that a rule change be allowed as part of the CAISO market redesign.
- ORNL will make a presentation to the CAISO on the concept and request that the rule change be considered as part of the market redesign. In addition, we will establish the needed frequency response criteria, i.e., the frequency droop setpoint and response time.
- At this point, the path would be made clear for the CDWR to implement the change in the rule redesign. Based on whether the rule change is for a 30-minute or 2-hour minimum, the CDWR would select which pumps to use in a pilot program.
- Funding would be obtained to make needed software changes to the SCADA system for the CAISO spinning reserve requirements, operational procedures would be modified, and the program would be initiated. If needed, soft starters will be installed.
- ORNL would monitor the program and prepare a final report.



## REFERENCES

- CAISO (California Independent System Operator) 2000, *FERC Electric Tariff, First Replacement Volume No. 1*, California Independent System Operator Corporation, October 13.
- CAISO (California Independent System Operator) 2003a, <http://oasis.caiso.com/>
- CAISO (California Independent System Operator) 2003b, [www.caiso.com](http://www.caiso.com)
- CAISO (California Independent System Operator) 2003c, “Actual Operating Reserves: Frequently Asked Questions,” <http://www1.caiso.com/docs/09003a6080/17/04/09003a60801704db.pdf>
- Hoffman 2003, personal communication between Brendan Kirby, ORNL, and Kyle Hoffman, CAISO Market Services.
- NERC (North American Electric Reliability Council) 2002, *NERC Operating Manual*, Princeton, New Jersey, November 21.
- FERC (U.S. Federal Energy Regulatory Commission) 2002a, *Notice of Proposed Rulemaking: Remediating Undue Discrimination through Open Access Transmission Service and Standard Electricity Market Design*, Docket No. RM01-12-000, Washington, D.C., July 31.
- WECC (Western Electricity Coordinating Council) 2002, *Reliability Criteria, Part III—Minimum Operating Reliability Criteria*, Salt Lake City, Utah, August.



**APPENDIX A**  
**SIEMENS TECHNICAL CONCEPT AND BUDGETARY ESTIMATE FOR PUMP**  
**MOTOR STARTING FREQUENCY CONVERTER**





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## Technical Concept and Budgetary Estimate

### Starting Frequency Converter system for Water Pumps

#### Oak Ridge National Laboratory for California Dept. of Water Resources

#### 1. Basis of proposal

The use of a Starting Frequency Converter (SFC) for starting synchronous motors driving water pumps is being considered for 2 pumping stations:

##### Chrisman (Wind Gap) synchronous motor data:

Qty. **6** each **44,000 HP**, 360 rpm, 13.2 kV, 1,540 A, 3 ph., 60 Hz, PF 0.95, Field 125 V, 930 A

Qty. **3** each **22,000 HP**, 514 rpm, 13.2 kV, 774 A, 3 ph., 60 Hz, PF 0.95, Field 125 V, 580 A

##### Teerink (Wheeler Ridge) synchronous motor data:

Qty. **6** each **20,000 HP**, 277 rpm, 13.2 kV, 704 A, 3 ph., 60 Hz, PF 0.95, Field 125 V, 721 A

Qty. **3** each **10,000 HP**, 400 rpm, 13.2 kV, 355 A, 3 ph., 60 Hz, PF 0.95, Field 125 V, 325 A

This concept and budgetary estimate is based on the following assumptions:

- Existing synchronous motors will be retained.
- Existing 13.2 kV switchgear (motor feeders) and all protection/control for operation will be retained.
- Existing field excitation equipment will be retained. This equipment includes an analog or digital controller (regulator) that allows control of the motor field current via a reference signal (4 to 20 mA, 0 to 10V or similar) from the SFC equipment.
- The motors/pumps will be started under no load as at present, i.e. pumps are emptied of water and the only the moment of inertia of the rotating parts determines the starting torque.

It may be possible for the SFC to start the pumps filled with water, but this would require further study.

We can of course offer additional equipment, such as new field exciters, if preferred.

Based on previous experience, we estimate that the SFC rating needs to be approximately 15% to 20% of the motor rating, i.e. approximately 5 MW to 7 MW for the 44,000 HP pumps. However, further information of the torque during starting is required, especially about breakaway torque for vertical pumps such as this.

The standard SFC ratings manufactured include units of 4 MW and 9 MW. We are basing this proposal on our 9 MW unit and expect that this will prove suitable after more detailed study.

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## 2. Description of proposed SFC system scope of supply

The proposed system comprises the following major components:

- SFC input (feeder) circuit breaker 13.2 kV, 2,000 A from existing 13.2 kV bus, with suitable protection for drive isolation transformer (motor protection relay).
- Drive isolation (SFC input) transformer: 12 MVA/2x 6 MVA, 13.2 kV Delta/2x 2.3 kV Delta/Wye, outdoor mineral oil filled.
- SFC unit comprising 12-pulse rectifier, DC link reactors, 6-pulse inverter with:
  - digital regulator
  - output for field current reference value
  - synchronizing unit, to synchronize SFC output voltage & frequency (phase) to the 60 Hz supply.
  - remote I/O units (via Profibus DP) for mounting in each of 9 existing field excitation units, for field current reference output and control/interlocking signals
  - PLC for selecting motor/pump to be started, control of new SFC output circuit breakers and existing motor feeder circuit breakers.

Air cooled, for indoor installation.

- OPTIONAL e-house (container type) for outdoor installation of SFC.
- SFC output transformer 12 MVA, 4.6 kV/13.2 kV, Delta/wye, outdoor mineral oil filled.
- De-magnetizing unit for SFC output transformer.
- SFC output switchgear, qty. 11 circuit breakers (1 per motor (=9), connected in parallel to existing motor feeder circuit breaker) each 13.2 kV, 2,000 A, with 2,000 A bus, 1 SFC output breaker/disconnect, 1 magnetizing unit breaker)

Please also refer to the attached system diagram.

Our scope of supply includes the design, manufacture and supply of the equipment listed, delivered ex works, domestic packaging.

Documentation includes drawings such as block diagrams, circuit diagrams etc. for the various pieces of equipment, standard operating and maintenance manuals.

### **Exclusions:**

- Tests other than routine production tests
- Installation engineering or design and associated drawings – plant layouts, cable specification, cable routing.
- Interface to the existing equipment, any modifications of existing equipment.
- Transportation to site
- Installation of equipment, supply, installation, connection of cables
- Start-up of the equipment, performance testing.

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### 3. Functional description:

The following sequence is applicable to starting a pump:

1. All motor feeder circuit breakers are open, the pump is stationary.
2. The SFC is powered up, ready to start.
3. The pump to be started is selected on the SFC. (This causes the relevant remote I/O unit for the motor field exciter and the respective motor feeder and SAFC output circuit breakers to be selected, and the SFC to be parameterized for the specific motor rating/type).
4. The pump needs to be prepared for starting as in the past (closing valves, evacuation of water etc.) It may be possible to initiate this from the new PLC, depending on the existing control system/equipment. When ready:
5. A "Start motor" command is given on the SFC. The SFC will:
  - 5.1. Close the SFC output circuit breaker.
  - 5.2. Command the field exciter to pulse the motor field current, and calculate the actual rotor position based on the measured induced stator voltages.
  - 5.3. Enable the SFC regulator, to start and ramp up the motor according to a preset speed/time ramp.
    - At low speeds (<10% or 15%) the DC link current is pulsed to allow the inverter to switch the current to the respective motor winding.
    - At higher speeds the motor back EMF allows the inverter to commutate naturally. The SFC controls the motor field current for the motor to operate at the required leading power factor.
6. When the motor is operating close to full speed (60 Hz), the synchronizing units causes the SFC output to be controlled such that it matches the 13.2 kV 60 Hz main supply. Once both voltage and phases are matched, the SFC control closes the (existing) motor feeder circuit breaker, and then blocks the SFC regulator and opens the SFC output circuit breaker. The pump motor is now connected across the line.
7. The existing pump control now brings the pump on line as at present (by opening the pump inlet valve, waiting for the pressure to match the system pressure, and then opening the outlet valve etc.).
8. Also, the SFC switches the demagnetizing unit to the 13.2 kV side of the output transformer.

The output transformer is demagnetized, because remanent magnetism in this transformer will distort the measurement of the rotor position detection as per 5.2 above.
9. Once the demagnetizing cycle is complete, the demagnetizing breaker (or contactor) is opened, and the SFC is ready to start the next motor.

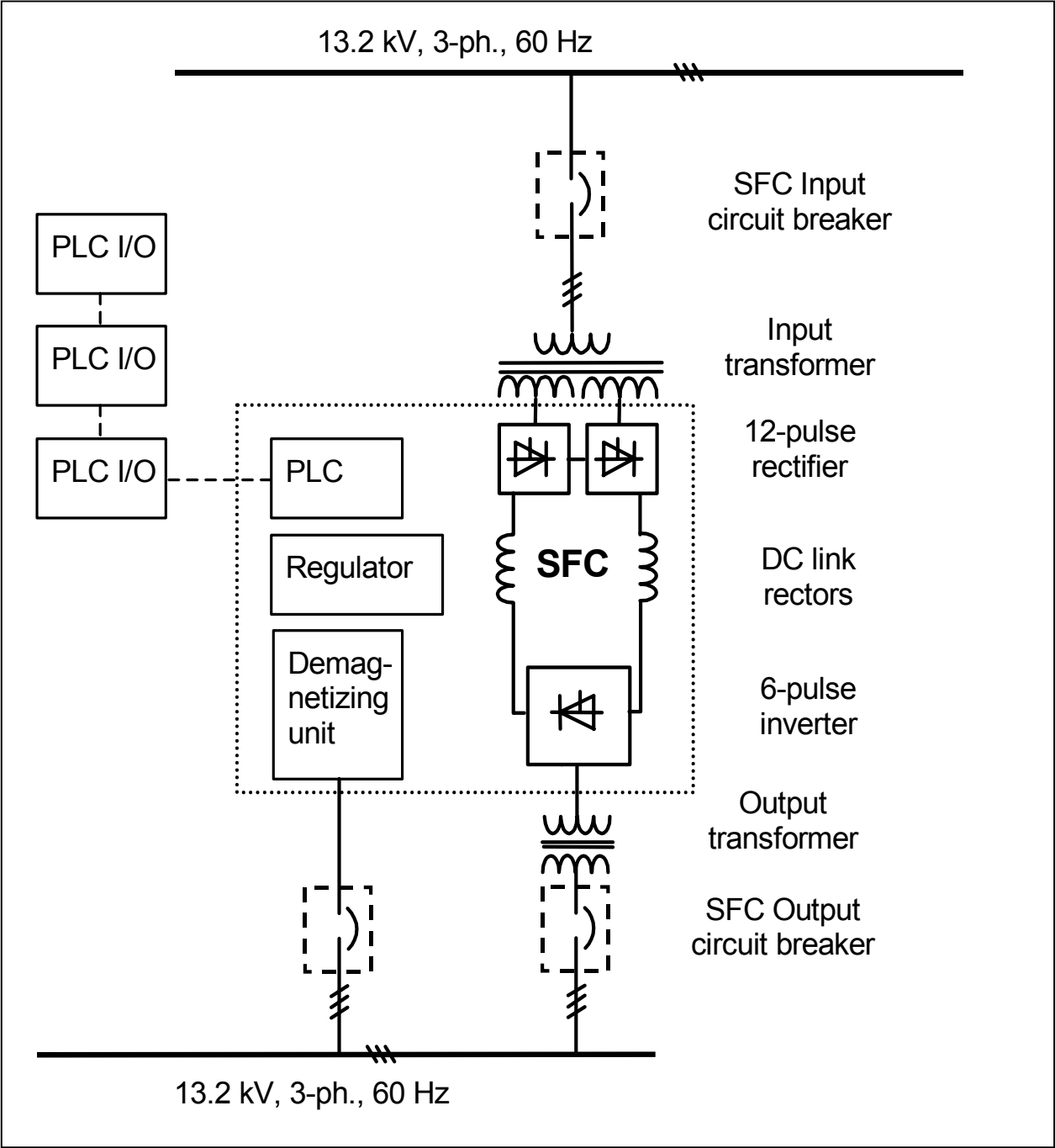
#### 4. Budgetary price estimate:

		<b>Budgetary price, each SFC system</b>
1	SFC input (feeder) circuit breaker 13.2 kV, 2,000 A	\$50,000.-
2	Transformers, outdoor mineral oil filled: SFC input 12 MVA/2x 6 MVA, 13.2 kV Delta/2x 2.3 kV Delta/Wye, SFC output 12 MVA, 4.6 kV/13.2 kV, Delta/wye	\$400,000.-
3	SFC unit air cooled, for indoor installation, comprising 12-pulse rectifier, DC link reactors, 6-pulse inverter with digital regulator, output for field current reference value, synchronizing unit, remote I/O units for existing field excitation units, PLC, de-magnetizing unit	\$450,000.-
4	OPTIONAL e-house (container type) for outdoor installation of SFC.	\$80,000.-
5	SFC output switchgear, 11 circuit breakers each 13.2 kV, 2,000 A, with 2,000 A bus	\$550,000.-
	Total budgetary estimate for <b>one</b> SFC system	<b>\$1,530,000.-</b>
	Budgetary estimate for 2nd SFC system	\$1,470,000.-
	Total budgetary estimate for <b>two</b> SFC systems	<b>\$3,000,000.-</b>

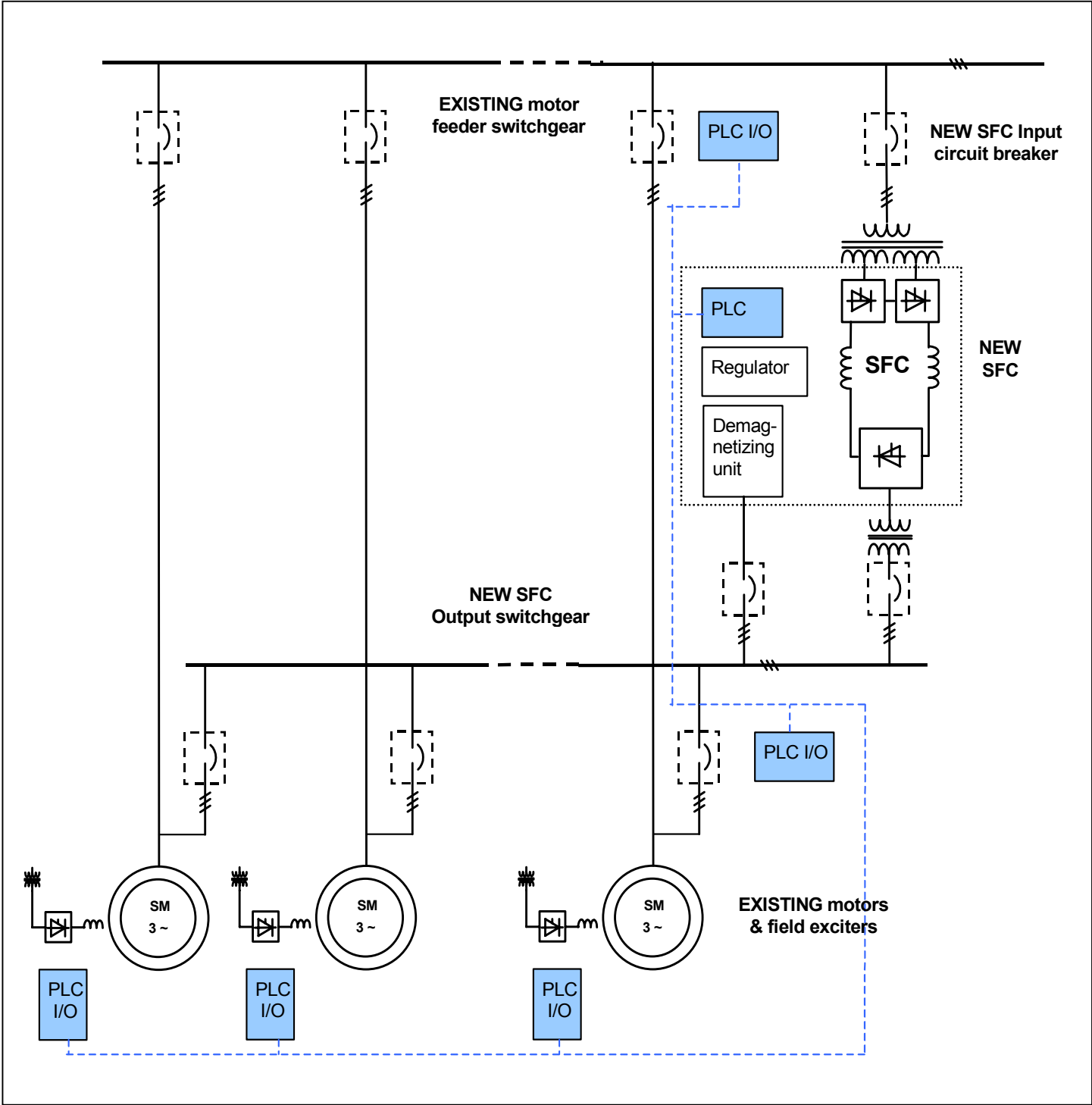
Note:

- The SFC equipment above is suitable for the Chrisman (Wind Gap) plant with 44,000 HP motors.
- This will also be suitable for the smaller ratings at Teerink (Wheeler Ridge), although it is oversized. It may be advantageous to use identical equipment for both sites, for spare parts and other reasons.
- Alternatively, it may be possible to lower the price by using smaller equipment at Teerink (for example transformers at approx. 50% rating, circuit breakers 1200 A instead of 2,000 A, even a smaller SFC). There will be some cost savings, but also additional costs for engineering a different system, loss of manufacturing efficiencies/price gained by producing two identical units etc.

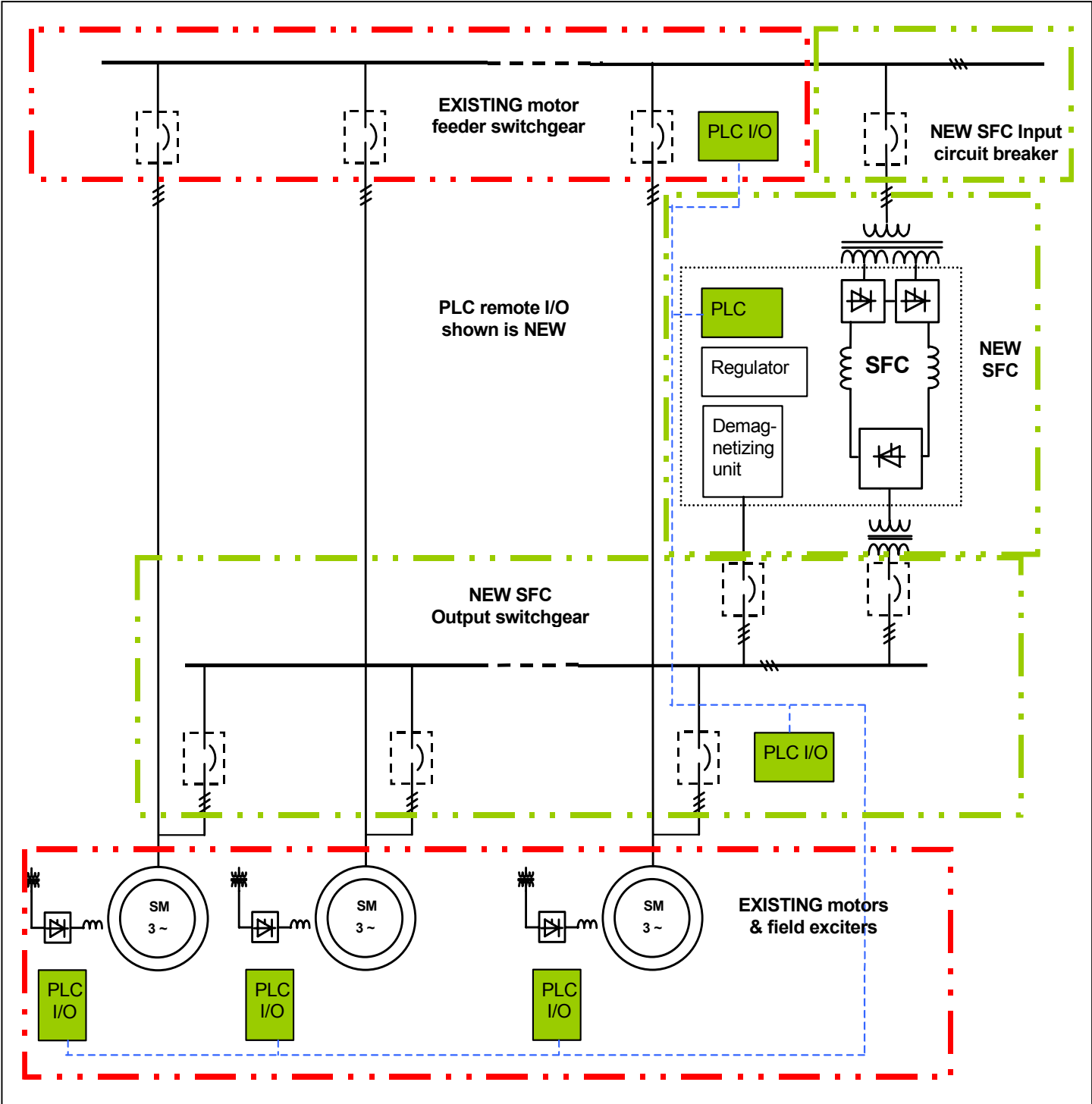
5 SFC block diagram



**6 Pump Station SFC system block diagram**



**7 Pump Station SFC system block diagram (2) indicating existing & new equipment**







**APPENDIX B**  
**SPINNING AND NON-SPINNING REVENUE PER PUMP**

Table B.1 presents modeling results for each individual pump supplying spinning reserves. Results are sorted by total annual revenue in the left three columns and by revenue per megawatt of pumping capacity in the right three columns. There is a \$1/MWh minimum price below which the pump does not provide reserve.

**Table B.1. Individual pump annual spinning reserve revenue**

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	Revenue \$/year	Pumping station	Pump number	Revenue \$/MW/year
1	ED	1	1,077,986	SB	1	29,620
2	ED	2	941,749	SB	2	29,572
3	ED	3	885,733	SB	3	28,354
4	ED	4	778,787	PO	1	28,163
5	DA	1	656,991	DE	1	28,101
6	ED	5	631,161	BL	1	27,928
7	BA	3	490,387	BS	1	27,807
8	ED	6	485,937	CR	1	27,716
9	ED	7	419,431	BH	1	27,542
10	BA	4	418,137	CR	2	26,385
11	BA	5	352,082	BS	2	26,061
12	ED	8	335,661	BH	2	25,703
13	BA	6	292,668	SB	4	24,129
14	DA	2	286,134	BA	1	23,333
15	ED	9	269,792	BH	3	22,966
16	WG	1	241,352	VJ	1	22,497
17	BA	7	240,550	BA	2	22,336
18	WG	2	216,768	BS	3	21,110
19	BA	1	205,910	DA	1	20,988
20	BA	2	197,111	SB	5	20,255
21	ED	10	195,656	BH	4	20,117
22	WG	4	160,089	BA	3	18,180
23	ED	11	136,623	BL	2	17,463
24	WG	3	126,844	DE	2	17,398
25	WR	1	114,639	PO	2	17,343
26	PB	1	113,647	ED	1	17,341
27	BV	1	113,411	BV	1	17,028
28	PB	3	105,805	CR	3	16,396
29	BV	2	103,883	SB	6	16,334
30	WR	2	102,506	BV	2	15,597
31	ED	12	98,486	BA	4	15,501
32	BA	8	92,792	ED	2	15,150
33	PB	2	92,228	BS	4	14,975
34	DA	3	80,580	BH	5	14,972
35	BV	4	68,557	WR	1	14,753
36	SB	5	62,956	ED	3	14,249
37	WR	4	62,684	WG	1	14,027
38	SB	2	57,446	WR	2	13,192

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	Revenue \$/year	Pumping station	Pump number	Revenue \$/MW/year
39	BV	3	55,998	BA	5	13,053
40	SB	3	55,081	OS	1	13,011
41	ED	13	55,014	SB	7	12,623
42	WR	3	52,158	WG	2	12,599
43	SB	6	50,768	ED	4	12,528
44	OS	5	48,873	PB	1	12,485
45	OS	1	47,662	VJ	2	11,702
46	SB	4	46,873	BA	6	10,850
47	SB	7	39,233	OS	2	10,584
48	PO	1	39,078	ED	5	10,153
49	DE	1	38,992	PB	2	10,132
50	OS	2	38,769	OS	3	9,259
51	BL	1	38,751	DA	2	9,141
52	WG	5	37,075	BA	7	8,918
53	BH	5	35,151	BV	3	8,408
54	BA	9	34,752	OS	4	8,021
55	OS	3	33,916	ED	6	7,817
56	SB	1	29,591	WG	3	7,372
57	OS	4	29,384	ED	7	6,747
58	BL	2	24,231	WR	3	6,712
59	DE	2	24,140	SB	8	6,124
60	PO	2	24,065	PB	3	6,014
61	BH	1	21,401	BS	5	5,612
62	BH	2	19,972	ED	8	5,400
63	BV	5	18,929	BV	4	5,147
64	BH	3	17,845	CR	4	5,145
65	PB	4	17,490	WG	4	4652
66	SB	8	16,655	ED	9	4340
67	WR	5	15,532	WR	4	4034
68	ED	14	13,453	BH	6	3802
69	BH	4	12,282	BA	8	3440
70	OS	6	12,229	DV	1	3392
71	BA	10	12,222	OS	5	3335
72	CR	2	11,422	ED	10	3147
73	CR	1	10,768	DA	3	2574
74	BS	3	9,725	VJ	3	2210
75	BH	6	8,926	ED	11	2198
76	CR	3	7,098	ED	12	1584
77	BS	4	6,982	BL	3	1482
78	BS	1	6,482	BV	5	1421
79	BS	2	6,075	BS	6	1415
80	VJ	1	3,122	PO	3	1393
81	BS	5	2,616	BA	9	1288
82	OS	7	2,389	DV	2	1166
83	CR	4	2,227	CR	5	1160
84	BV	6	2,195	WG	5	1077
85	BL	3	2,057	DE	3	1055
86	PO	3	1,933	WR	5	999

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	Revenue \$/year	Pumping station	Pump number	Revenue \$/MW/year
87	VJ	2	1,624	PB	4	994
88	DE	3	1,464	ED	13	885
89	SB	9	1,350	OS	6	835
90	WR	6	1,156	BS	7	576
91	WG	6	1,125	SB	9	496
92	CR	5	708	BA	10	453
93	MJ	1	672	DV	3	280
94	BS	6	660	ED	14	216
95	DV	1	659	BV	6	165
96	BA	11	656	OS	7	163
97	VJ	3	601	WR	6	74
98	BS	7	269	PO	4	65
99	DV	2	226	BL	4	65
100	DA	4	190	BL	5	60
101	PB	5	177	DE	4	59
102	DA	5	156	PO	5	59
103	PO	4	90	BL	6	59
104	BL	4	90	DE	5	59
105	BL	5	83	DE	6	58
106	DE	4	82	PO	6	54
107	PO	5	82	CR	6	52
108	BL	6	82	WG	6	33
109	DE	5	82	BA	11	24
110	DE	6	81	BS	8	17
111	PO	6	75	PB	5	10
112	DV	3	54	DA	4	6
113	DA	6	50	BS	9	5
114	CR	6	32	DA	5	5
115	BV	8	15	DA	6	2
116	BV	7	15	VJ	4	1
117	BS	8	8	BV	8	1
118	BV	9	3	BV	7	1
119	BS	9	2	CR	7	0
120	WG	7	1	BV	9	0

Table B.2 presents modeling results for each individual pump supplying non-spinning reserves. Results are sorted by total annual revenue in the left three columns and by revenue per megawatt of pumping capacity in the right three columns. There is a minimum \$1/MWh price below which the pump does not provide reserves.

**Table B.2. Individual pump annual non-spinning reserve revenue**

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	Revenue \$/year	Pumping station	Pump number	Revenue \$/MW/year
1	ED	1	443,084	SB	1	13,722
2	ED	2	356,037	SB	2	13,713

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	\$/year	Pumping station	Pump number	\$/MW/year
3	ED	3	328,684	PO	1	13,343
4	DA	1	327,147	SB	3	13,341
5	ED	4	279,485	DE	1	13,323
6	BA	3	239,965	BS	1	13,259
7	BA	4	212,549	BL	1	13,235
8	ED	5	211,920	CR	1	13,229
9	BA	5	182,814	BH	1	13,028
10	DA	2	178,313	CR	2	12,796
11	ED	6	157,104	BS	2	12,696
12	BA	6	145,793	BH	2	12,259
13	BA	7	119,960	SB	4	12,224
14	ED	7	119,611	VJ	1	11,419
15	BA	1	100,540	BA	1	11,393
16	BA	2	98,181	BH	3	11,177
17	WG	1	92,256	BA	2	11,125
18	ED	8	82,704	BS	3	11,062
19	WG	2	77,931	SB	5	10,895
20	ED	9	67,781	DA	1	10,451
21	DA	3	55,554	BH	4	10,302
22	BV	1	48,338	SB	6	9,280
23	ED	10	47,833	BA	3	8,896
24	PB	1	46,020	BS	4	8,702
25	WG	4	44,451	BL	2	8,698
26	BV	2	43,447	DE	2	8,646
27	WR	1	43,393	PO	2	8,608
28	WG	3	41,671	CR	3	8,385
29	WR	2	37,497	BH	5	8,353
30	BA	8	37,232	BA	4	7,880
31	PB	3	36,609	SB	7	7,304
32	PB	2	35,568	BV	1	7,258
33	SB	5	33,862	ED	1	7,128
34	SB	6	28,843	BA	5	6,777
35	ED	11	28,520	BV	2	6,523
36	SB	2	26,638	VJ	2	6,459
37	SB	3	25,917	ED	2	5,727
38	SB	4	23,747	DA	2	5,696
39	SB	7	22,700	WR	1	5,584
40	ED	12	20,731	BA	6	5,405
41	BV	4	20,011	WG	1	5,362
42	BH	5	19,611	ED	3	5,287
43	PO	1	18,515	PB	1	5,056
44	DE	1	18,487	WR	2	4,826
45	BL	1	18,365	OS	1	4,719
46	BV	3	18,217	WG	2	4,529
47	OS	1	17,288	ED	4	4,496
48	WR	4	16,115	BA	7	4,447
49	WR	3	15,839	PB	2	3,908
50	SB	1	13,709	OS	2	3,647

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	\$/year	Pumping station	Pump number	\$/MW/year
51	OS	2	13,360	BS	5	3,591
52	OS	5	12,545	SB	8	3,511
53	BL	2	12,069	ED	5	3,409
54	DE	2	11,997	OS	3	3,070
55	PO	2	11,944	CR	4	2,881
56	OS	3	11,244	BV	3	2,735
57	BH	1	10,123	OS	4	2,532
58	SB	8	9,548	ED	6	2,527
59	BH	2	9,526	WG	3	2,422
60	OS	4	9,275	BH	6	2,084
61	BA	9	9021	PB	3	2,081
62	ED	13	8967	WR	3	2,038
63	BH	3	8685	ED	7	1,924
64	WG	5	8451	DA	3	1,775
65	BH	4	6290	DV	1	1563
66	CR	2	5540	BV	4	1502
67	CR	1	5140	BA	8	1380
68	BS	3	5096	ED	8	1330
69	BH	6	4893	WG	4	1292
70	PB	4	4870	VJ	3	1232
71	BV	5	4328	ED	9	1090
72	BS	4	4057	WR	4	1037
73	CR	3	3630	BS	6	998
74	BS	1	3091	OS	5	856
75	BS	2	2960	ED	10	769
76	BA	10	2880	CR	5	702
77	OS	6	2537	BL	3	607
78	WR	5	2415	PO	3	537
79	BS	5	1674	ED	11	459
80	VJ	1	1584	DV	2	454
81	ED	14	1412	DE	3	392
82	CR	4	1247	SB	9	345
83	SB	9	937	BA	9	334
84	VJ	2	896	ED	12	333
85	BL	3	843	BV	5	325
86	PO	3	746	BS	7	323
87	PF	1	620	PB	4	277
88	DE	3	544	WG	5	246
89	BS	6	465	OS	6	173
90	BV	6	432	WR	5	155
91	CR	5	428	ED	13	144
92	VJ	3	335	BA	10	107
93	WG	6	330	DV	3	93
94	DV	1	304	CR	6	38
95	OS	7	264	BV	6	32
96	BA	11	175	BL	4	31
97	BS	7	151	PO	4	24
98	DV	2	88	DE	4	23

Rank	Total revenue			Revenue/MW-pump-capacity		
	Pumping station	Pump number	\$/year	Pumping station	Pump number	\$/MW/year
99	BL	4	43	ED	14	23
100	PO	4	34	BL	5	20
101	DE	4	32	PO	5	19
102	BL	5	27	BL	6	19
103	PO	5	27	DE	5	19
104	BL	6	27	DE	6	19
105	DE	5	27	OS	7	18
106	DE	6	26	PO	6	18
107	PO	6	25	WG	6	10
108	CR	6	23	BA	11	6
109	DV	3	18	BS	8	2
110	PB	5	18	PB	5	1
111	WR	6	11	WR	6	1